Secretariat of the Team for Countermeasures for Decommissioning and Contaminated Water Treatment

Main decommissioning work and steps

Fuel removal from the Unit 4 SFP was completed on December 22, 2014 and removal from the Unit 3 SFP has been underway since April 15, 2019. Dust density in the surrounding environment is being monitored and work is being implemented with safety first. Work continues sequentially toward the start of fuel removal from Units 1 and 2 and debris (Note 1) retrieval

from Units 1-3. Units 1 & 2 (Note 1) Fuel assemblies having melted through in the accident. Unit 3 Unit 4 Unit 1: Fuel removal scheduled to start in FY2023 Installing **Fuel Removal** Rubble removal Storage and Unit 2: Fuel removal scheduled to start in FY2023 Fuel removal Fuel removal Unit 3: Fuel removal scheduled to start around mid-FY2018* from SFP & dose reduction handling machine Unit 4: Fuel removal completed in 2014 * Fuel removal started from April 15, 2019. Unit 1-3 Ascertaining the status inside the PCV (Note 2) **Fuel Debris** Storage and **Fuel debris** The method employed to retrieve fuel examining the fuel debris retrieval debris from the first unit will be Retrieval handling retrieval confirmed in FY2019. method, etc. (Note 2) Scenario Design and **Dismantling** development manufacturing **Dismantling** & technology of devices / **Facilities** consideration equipment

Fuel removal from the spent fuel pool

Toward fuel removal from the Unit 1 spent fuel pool, investigations have been implemented to ascertain the conditions of the fallen roof on the south side and the contamination of the well plug. Based on the results of these investigations, "the method to initially install a large cover over the Reactor Building and then remove rubble inside the cover" was selected to ensure a safer and more secure removal. Details of the selected method will be designed and the process of fuel removal will be refined.

<Reference> Progress to date

Rubble removal on the north side of the operating floor started from January 2018 and has been implemented sequentially. In July and August 2019, the well plug, which was

misaligned from its normal position, was investigated and in August and September, the conditions of the overhead crane were checked. Based on the results of these investigations, as the removal requires more careful work taking dust scattering into consideration, two methods were examined: installing a cover after rubble removal and initially installing a large cover over the Reactor Building and then removing rubble inside the cover

Initially installing a large cover for fuel removal (image)

Three principles behind contaminated water countermeasures

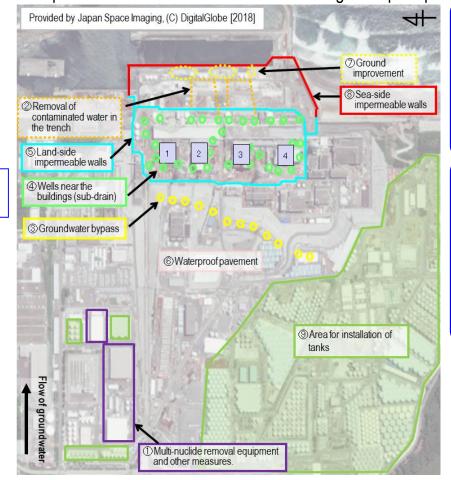
Countermeasures for contaminated water are implemented in accordance with the following three principles:

1 **Remove** contamination sources

- 1 Purification using Multi-nuclide removal equipment and other measures
- ② Removal of contaminated water from the trench (Note 3)

(Note 3) Underground tunnel containing pipes.

- 2. Redirect groundwater from contamination sources
- 3 Pump up groundwater for bypass
- 4 Pump up groundwater near buildings
- 5 Land-side impermeable walls (frozen-soil walls)
- 6 Waterproof pavement
- 3. Prevent leakage of contaminated water
- Tenhance soil by adding sodium silicate
- 8 Sea-side impermeable walls
- (9) Increase the number of (welded-joint) tanks



Multi-nuclide removal equipment (ALPS), etc.

- This equipment removes radionuclides from the contaminated water in tanks and reduces risks.
- Treatment of contaminated water (RO concentrated salt water) was completed in May 2015 with multi-nuclide removal equipment, additional multi-nuclide removal equipment installed by TEPCO (operation commenced in September 2014) and a Japanese Government subsidy project (operation commenced in October 2014).
- Strontium-treated water from equipment other than ALPS is being re-treated



(High-performance multi-nuclide removal equipment)

Reducing the generation of contaminated water through multi-layered measures

- Multi-layered measures are implemented to suppress the inflow of rainwater and groundwater into buildings
- Multi-layered contaminated water management measures, including land-side impermeable walls and subdrains, have stabilized the groundwater at a low level. The increase in the amount of contaminated water generated during rainfall is being suppressed by repairing damaged portions of building roofs, facing onsite, etc.
- Through these measures, the generation of contaminated water was reduced from approx. 470 m³/day (in FY2014) to approx. 170 m³/day (in
 - The groundwater level around Unit 1-4 Reactor Buildings will remain limited by steadily operating land-side impermeable walls. In addition, measures to prevent the inflow of rainwater, including repairing damaged parts of building roofs and facing, continue to reduce the generation of contaminated water still further.



Inside the land-side Outside the land-side impermeable wall impermeable wall

Replacing flanged tanks with welded-joint tanks

- Flanged tanks are being replaced with more reliable welded-joint tanks.
- Strontium-treated water stored in flanged tanks was purified and transferred to welded-joint tanks. The transfer was completed in November 2018. Transfer of ALPS-treated water was completed in March 2019.



(Installed welded-joint tanks)

Progress Status and Future Challenges of the Mid-and-Long-Term Roadmap toward Decommissioning of TEPCO Holdings Fukushima Daiichi Nuclear Power Station (Outline)

Progress status

- ◆ The temperatures of the Reactor Pressure Vessel (RPV) and Primary Containment Vessel (PCV) of Units 1-3 have been maintained within the range of approx. 20-30°C*1 over the past month. There was no significant change in the density of radioactive materials newly released from Reactor Buildings into the air*2. It was concluded that the comprehensive cold shutdown condition had been maintained.
- 1 The values varied somewhat, depending on the unit and location of the thermometer
- * 2 In November 2019, the radiation exposure dose due to the release of radioactive materials from the Unit 1-4 Reactor Buildings was evaluated at less than 0.00007 mSv/year at the site boundary. The annual radiation dose from natural radiation is approx. 2.1 mSv/year (average in Japan).

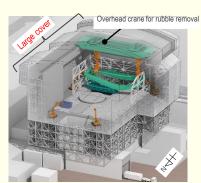
Selection of the method to initially install a large cover and remove rubble inside the cover for Unit 1

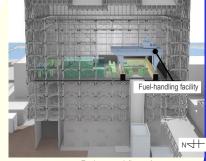
Toward fuel removal from Unit 1, two methods were examined: (i) installing a cover after rubble removal and (ii) initially installing a large cover over the Reactor Building and then removing rubble inside the cover...

Following the examination, "the method to initially install a large cover over the Reactor Building

and then remove rubble inside the cover" was selected to ensure a safer and more secure removal.

Details of the selected method will be designed and the fuel removal process will be refined.

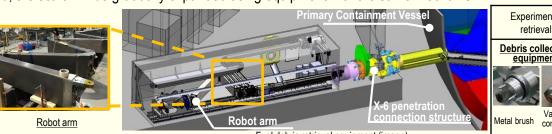




Evaluated that Unit 2 is suitable for the first implementing unit for fuel debris retrieval

For fuel debris retrieval from the first implementing unit, methods have been examined; taking the progress status in internal investigations of the Primary Containment Vessel (PCV), the status of improvement in the work environment and other factors into consideration.

The characteristics of the debris acquired by the contact investigation in February 2019 and, the status of improvement in the environment on the 1st floor of the Reactor Building for access to PCV and the engineering works with these results taken into consideration and Unit 2 was evaluated that it is suitable for the first implementing unit for fuel debris retrieval. As the method, to determine, a trial retrieval using a robot arm will begin. After verifying and checking this retrieval method, the scale will be gradually expanded using equipment with the same mechanism.



Experimental Gradual expansion of retrieval the retrieval scope Debris collection Debris collection equipment Vacuum

Fuel debris retrieval equipment (image) Cover for fuel removal Blowout panel (closed) Operating floor Transferred fuel (assemblies)*1 Front chamber Dome roof Removed fuel (assemblies) **28/566** _Fuel-handling Windbreak **1535**/1535*2 Spent Fuel Pool (As of July 21, 2019) fence on December 22, 2014) Primary ontainmen 615 392 Water Water Water injection Reactor injection Pressure Vessel (RPV) March 31, 201 **1568**/1568 Unit 4^{* 2} Including two new fuel assemblies removed first in 2012. Unit 3 *1 Fuel assemblies stored in the rack of the common pool Reactor Building (R/B) Unit 1 Unit 2

Unit 1 Unit 2 Dose at the Slightly high (approx. 10mSv/h Containment o (no hydrogen Slightly high Low airtightness Condition of Information ohtained Access route Removal of high Decrease of wate dose pipes is

Comparison of each unit

Dismantling for the 5th block of the Unit 1/2 exhaust stack

For the Unit 1/2 exhaust stack, dismantling of the 4th block was completed on December 4 and the subdrain suspended due to interference

of the work was recovered on December 6.

Based on the following review of work to date and refining of the whole process, dismantling is estimated to be completed around early May in 2020*

Dismantling of the 5th block started from December 16 and was completed on December 19.

* As spare dates for bad weather, trouble of equipment and other accidents are not considered, the estimated date may change



Progress status in dismantling of the exhaust stack

Check of the conditions of sandbags installed on the basement floor of the HTI Building

To check the conditions of Zeolite sandbags installed on the basement floor of the High Temperature Incinerator (HTI) Building as a contaminated water treatment measure immediately after the earthquake, a dose investigation using an underwater drone and a visual inspection started from December 3.

The investigation confirmed that sandbags were broken and confirmed that the maximum surface dose of sandbags within the investigative scope was 4,000 mSv/h.

Based on the investigative results, the dose effect when will be assessed



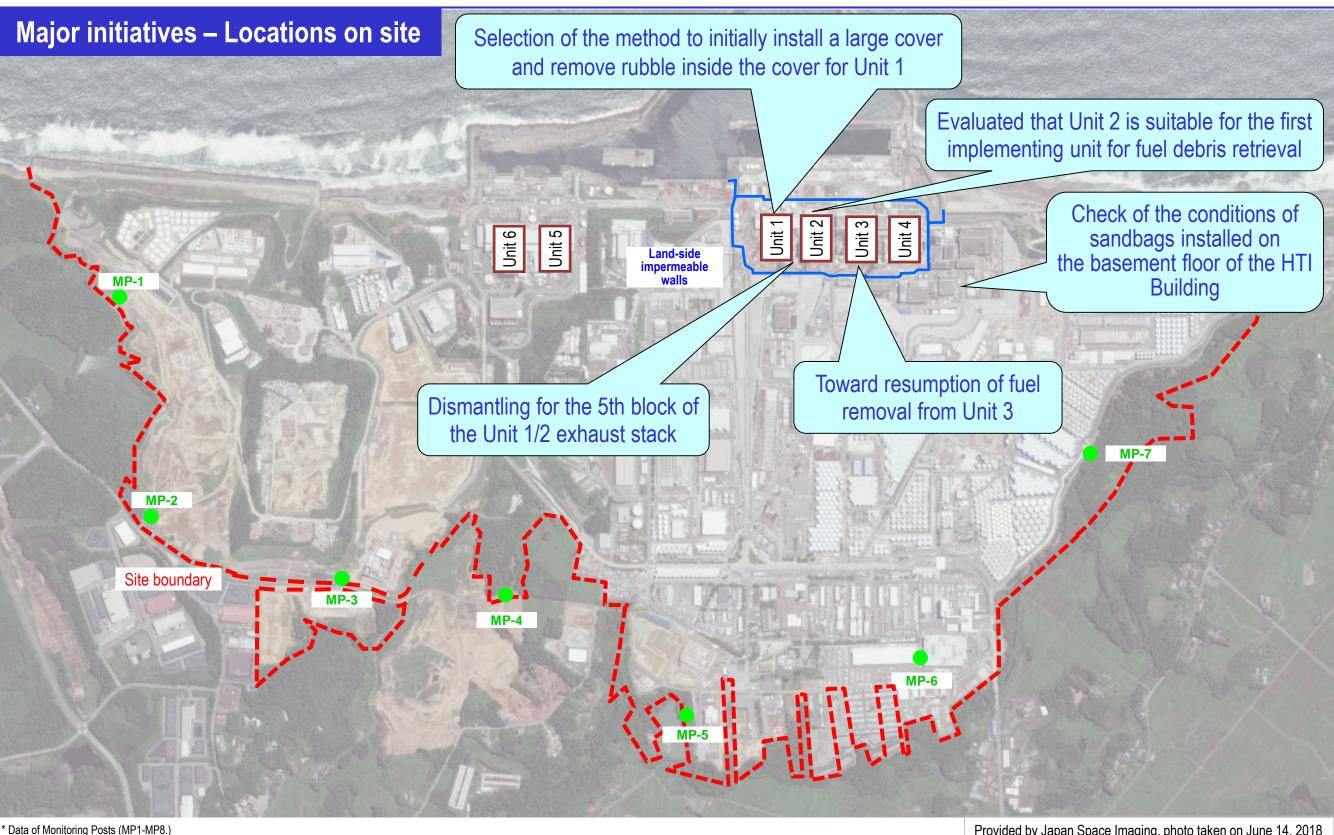
the basement floor is exposed Condition immediately after the earthquake



Toward resumption of fuel removal from Unit 3

Measures were implemented for defects detected during the preparatory work toward resumption of fuel removal from Unit 3 and operation was checked using dummy fuel. On December 14. however, interference of cans inside the transportation cask and dummy fuel was identified.

Though the following investigation confirmed slight leaning of the FHM mast, measures. including a review of the procedures, will be implemented to complete fuel removal within FY2020.



Therefore, monitoring results at these points are lower than elsewhere in the power plant site.

The radiation shielding panels around monitoring post No. 6, which is one of the instruments used to measure the radiation dose at the power station site boundary, were taken off from July 10-11, 2013, since further deforestation, etc. had caused the surrounding radiation dose to decline significantly.

Provided by Japan Space Imaging, photo taken on June 14, 2018 Product(C) [2018] DigitalGlobe, Inc.

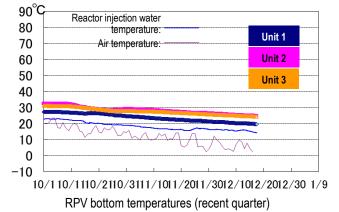
Data (10-minute values) of Monitoring Posts (MPs) measuring the airborne radiation rate around site boundaries showed 0.400 – 1.315 µSv/h (November 27 – December 17, 2019).

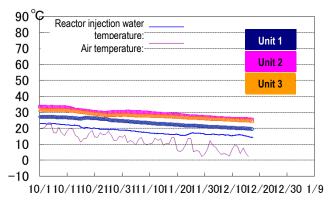
We improved the measurement conditions of monitoring posts 2 to 8 to measure the air-dose rate precisely. Construction work, such as tree-clearing, surface soil removal and shield wall setting, were implemented from February 10 to April 18, 2012.

I. Confirmation of the reactor conditions

1. Temperatures inside the reactors

Through continuous reactor cooling by water injection, the temperatures of the Reactor Pressure Vessel (RPV) bottom and the Primary Containment Vessel (PCV) gas phase were maintained within the range of approx. 20 to 30°C for the past month, though they varied depending on the unit and location of the thermometer.



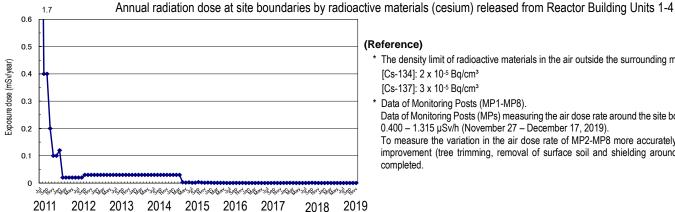


PCV gas phase temperatures (recent quarter)

* The trend graphs show part of the temperature data measured at multiple points.

2. Release of radioactive materials from the Reactor Buildings

As of November 2019, the density of the radioactive materials newly released from Reactor Building Units 1-4 into the air and measured at the site boundary was evaluated at approx. 1.9×10⁻¹² Bq/cm³ and 7.0×10⁻¹² Bq/cm³ for Cs-134 and Cs-137 respectively, while the radiation exposure dose due to the release of radioactive materials there was less than 0.00007 mSv/year.



- * The density limit of radioactive materials in the air outside the surrounding monitoring area: [Cs-134]: 2 x 10-5 Bq/cm³
- [Cs-137]: 3 x 10-5 Bg/cm3
- Data of Monitoring Posts (MP1-MP8).

Data of Monitoring Posts (MPs) measuring the air dose rate around the site boundary showed 0.400 - 1.315 µSv/h (November 27 - December 17, 2019).

To measure the variation in the air dose rate of MP2-MP8 more accurately, environmental improvement (tree trimming, removal of surface soil and shielding around the MPs) was

Note 1: Different formulas and coefficients were used to evaluate the radiation dose in the facility operation plan and monthly report. The evaluation methods were integrated in September 2012. As the fuel removal from the spent fuel pool (SFP) commenced for Unit 4, the radiation exposure dose from Unit 4 was added to the items subject to evaluation since November 2013. The evaluation has been changed to a method considering the values of continuous dust monitors since FY2015, with data to be evaluated monthly and announced the following month.

Note 2: Radiation dose was calculated using the evaluation values of release amount from Units 1-4 and Units 5 and 6. The radiation dose of Unit 5 and 6 was evaluated based on expected release amount during operation until September 2019 but the evaluation method was reviewed and changed to calculate based on the actual measurement results of Units 5 and 6 from October.

3. Other indices

There was no significant change in indices, including the pressure in the PCV and the PCV radioactivity density (Xe-135) for monitoring criticality, nor was any abnormality in the cold shutdown condition or criticality sign detected.

Based on the above, it was confirmed that the comprehensive cold shutdown condition had been maintained and the reactors remained in a stabilized condition.

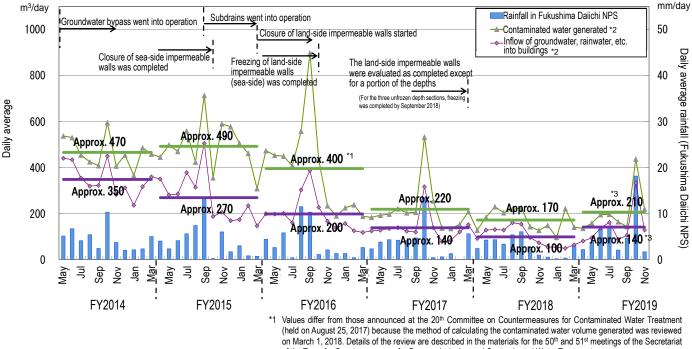
II. Progress status by each plan

1. Contaminated water management

In accordance with the three principles "remove" contamination sources, "redirect" groundwater from contamination sources and "prevent leakage" of contaminated water, multi-layered contaminated water management measures have been implemented to stably control groundwater

Status of contaminated water generated

- Multi-layered measures, including pumping up by subdrains and land-side impermeable walls, which were implemented to control the continued generation of contaminated water, suppress the groundwater inflow into buildings.
- Following the steady implementation of "redirecting" measures (groundwater bypass, subdrains, land-side impermeable walls and other measures), the generation amount reduced from approx. 470 m³/day (the FY2014 average) when the measures were first launched to approx. 170 m³/day (the FY2018 average).
- Measures will continue to further reduce the volume of contaminated water generated.



- of the Team for Countermeasures for Decommissioning and Contaminated Water Treatment *2: The monthly daily average is derived from the daily average from the previous Thursday to the last Wednesday, which
- is calculated based on the data measured at 7:00 on every Thursday *3: The average (provisional value) for the period April – November 2019
- Figure 1: Changes in contaminated water generated and inflow of groundwater, rainwater, into buildings

Operation of the groundwater bypass

- From April 9, 2014, the operation of 12 groundwater bypass pumping wells commenced sequentially to pump up groundwater. The release then started from May 21, 2014, in the presence of officials from the Intergovernmental Liaison Office for the Decommissioning and Contaminated Water Issue of the Cabinet Office. Up until December 17, 2019, 513,929 m³ of groundwater had been released. The pumped-up groundwater was temporarily stored in tanks and released after TEPCO and a third-party organization had confirmed that its quality met operational targets.
- Pumps are inspected and cleaned as required based on their operational status.

Operation of the Water Treatment Facility special for Subdrain & Groundwater drains

- To reduce the level of groundwater flowing into the buildings, work began to pump up groundwater from wells (subdrains) around the buildings on September 3, 2015. The pumped-up groundwater was then purified at dedicated facilities and released from September 14, 2015, in the presence of officials from the Intergovernmental Liaison Office for the Decommissioning and Contaminated Water Issue of the Cabinet Office. Up until December 17, 2019, a total of 826,869 m³ had been drained after TEPCO and a third-party organization had confirmed that its quality met operational targets.
- Due to the rising level of the groundwater drain pond after the sea-side impermeable walls had been closed, pumping started on November 5, 2015. Up until December 18, 2019, a total of approx. 225,644 m³ had been pumped up and a volume of under 10 m³/day is being transferred from the groundwater drain to the Turbine Buildings (average for the period November 21 – December 11, 2019).
- As one of the multi-layered contaminated-water management measures, in addition to waterproof pavement (facing:

as of the end of November 2019, approx. 94% of the planned area had been completed) to prevent rainwater infiltrating the ground, facilities to enhance the subdrain treatment system were installed and went into operation from April 2018, increasing the treatment capacity from 900 to 1,500 m³/day and improving reliability. Operational efficiency was also improved to treat up to 2,000 m³/day for almost one week during the peak period.

- To maintain the level of groundwater pumped up from the subdrains, work to install additional subdrain pits and recover
 those already in place is underway. The additional pits are scheduled to begin operation sequentially from a pit for
 which work was completed (12 of 14 pits went into operation). For recovered pits, work for all three pits scheduled
 was completed, all of which went into operation from December 26, 2018. Work to recover another pit started from
 November 2019 (No. 49 pit).
- To eliminate the need to suspend water pumping while cleaning the subdrain transfer pipe, the pipe will be duplicated. Installation of the pipe and ancillary facilities was completed.
- Since the subdrains went into operation, the inflow to buildings tended to decline to under 150 m³/day when the subdrain water level declined below T.P. 3.0 m but increased during rainfall.

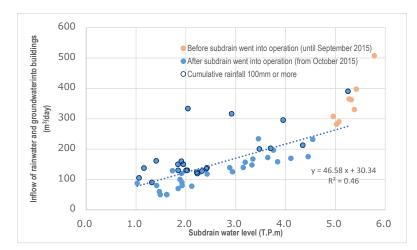


Figure 2: Correlation between inflow such as groundwater and rainwater into buildings and the water level of Units 1-4 subdrains

- Construction status of the land-side impermeable walls and status of groundwater levels around the buildings
- An operation to maintain the land-side impermeable walls and prevent the frozen soil from thickening further continued from May 2017 on the north and south sides and started from November 2017 on the east side, where sufficiently thick frozen soil was identified. The scope of the maintenance operation was expanded in March 2018.
- In March 2018, construction of the land-side impermeable walls was completed, except for a portion of the depth, based on a monitoring result showing that the underground temperature had declined below 0°C in almost all areas, while on the mountain side, the difference in internal and external water levels increased to approx. 4-5 m. The 21st Committee on Countermeasures for Contaminated-Water Treatment, held on March 7, 2018, evaluated that alongside the function of subdrains and other measures, a water-level management system to stably control groundwater and redirect groundwater from the buildings had been established and allowed the amount of contaminated water generated to be reduced significantly.
- A supplementary method was implemented for the unfrozen depth and it was confirmed that the temperature of this
 portion had declined below 0°C by September 2018. From February 2019, a maintenance operation started
 throughout all sections.
- The groundwater level in the area inside the land-side impermeable walls has been declining every year. On the mountain side, the difference between the inside and outside increased to approx. 4-5 m. The water level in the bank area has remained low (T.P. 1.6-1.7 m) compared to the ground surface (T.P. 2.5 m).

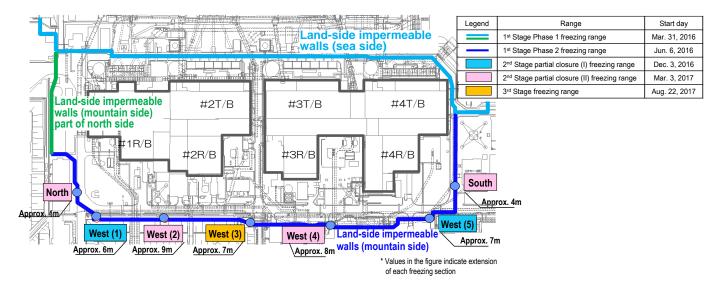


Figure 3: Closure parts of the land-side impermeable walls (on the mountain side)

Operation of multi-nuclide removal equipment

- Regarding the multi-nuclide removal equipment (existing and high-performance), hot tests using radioactive water were underway (for existing equipment, System A: from March 30, 2013, System B: from June 13, 2013, System C: from September 27, 2013; and for high-performance equipment, from October 18, 2014). The additional multi-nuclide removal equipment went into full-scale operation from October 16, 2017.
- As of December 12, 2019, the volumes treated by existing, additional and high-performance multi-nuclide removal equipment were approx. 422,000, 605,000 and 103,000 m³, respectively (including approx. 9,500 m³ stored in the J1(D) tank, which contained water with highly concentrated radioactive materials at the System B outlet of the existing multi-nuclide removal equipment).
- To reduce the risks of strontium-treated water, treatment using existing, additional and high-performance multi-nuclide removal equipment has been underway (existing: from December 4, 2015; additional: from May 27, 2015; high-performance: from April 15, 2015). Up until December 12, 2019, approx. 656,000 m³ had been treated.

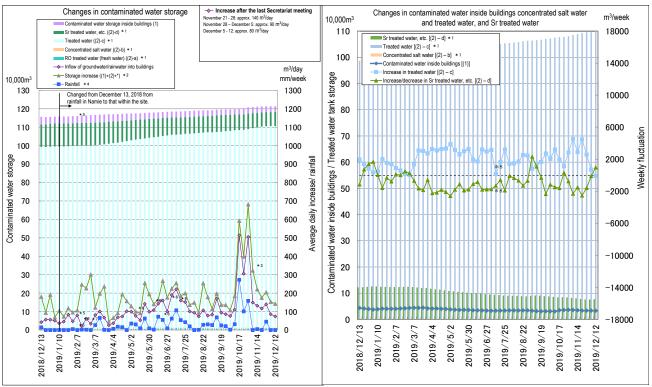
> Toward reducing the risk of contaminated water stored in tanks

Treatment measures comprising the removal of strontium by cesium-adsorption apparatus (KURION) (from January 6, 2015), the secondary cesium-adsorption apparatus (SARRY) (from December 26, 2014) and the third cesium-adsorption apparatus (SARRY II) (from July 12, 2019) have been underway. Up until December 12, 2019, approx. 557.000 m³ had been treated.

Measures in the Tank Area

• Rainwater, under the release standard and having accumulated within the fenced-in area of the contaminated-water tank area, was sprinkled on site after eliminating radioactive materials using rainwater-treatment equipment since May 21, 2014 (as of December 16, 2019, a total of 144,615 m³).

As of December 12, 2019



- *1: Water amount for which the water-level gauge indicates 0% or more
- *2: To detect storage increases more accurately, the calculation method was reviewed as follows from February 9, 2017: (The revised method was applied from March 1, 2018) [(Inflow of groundwater/rainwater into buildings) + (other transfer) + (chemical injection into ALPS)]
- *3: The storage amount increased due to transfer to buildings in association with the decommissioning work.

 (The transferred amount comprised (①Transfer of RO concentrated water from groundwater drains to Turbine Building: approx. 80 m³/day, ②Transfer from wells and groundwater drains: approx.50 m³/day, ③Transfer from Unit 51/6
- *4: Changed from December 13, 2018 from rainfall in Namie to that within the site.
- *5: Since January 17, 2019, Unit 3 C/B contaminated water has been managed in addition to contaminated water storage in buildings. For the inflow of groundwater, rainwater and others to buildings and increase in storage have been reflected since January 24, 2019.
- *6: Considered attributable to the increased inflow of groundwater, rainwater and others to buildings due to the decline in the level of contaminated water in buildings (January 17, April 22, May 16 and 30, June 13 and 27, 2019)
- *7: Water-level gauges were replaced (February 7 March 7, 2019)

SPT to Process Main Building; approx. 20 m3/day, others)

*8: Calculation methods for water volume and the capacity of tanks, which had varied in each tank area, were unified in all areas. By this unification, the calculated increase in treated water and variation in Sr-treated water and others changed. However, the actual treated volumes were approx. 2200 m³/week for treated water and approx. 1100 m³/week for Sr-treated water and others (July 11, 2019).

Figure 4: Status of contaminated water storage

> Amount of contaminated water generated (inflow to buildings) during heavy rain in 2019

- In October 2019, the largest rainfall after the earthquake, approx. 560 mm/month, was observed.
- Compared to the recent record in October 2017 when a similar level of rainfall was observed, the inflow to buildings
 during one week after the rainfall started reduced by about 3,000m³, showing the effect of measures to suppress
 inflow to buildings. In addition, inflow continued after the cessation of rainfall in 2017 but quickly reduced in 2019
 following the establishment of the land-side impermeable walls and enhancement of the subdrain treatment capability.
- Regarding inflow by unit, Unit 1 had an inflow corresponding to the damaged area of the building roof and Units 2 and 3 had even larger inflows.
- · Rainwater prevention measures for building roofs and facing will be implemented to suppress inflow.

Progress status of contaminated water treatment in buildings

- To check the conditions of Zeolite sandbags installed on the basement floor of the High Temperature Incinerator Building as a contaminated water treatment measure immediately after the earthquake, a dose investigation using an underwater drone and a visual inspection started from December 3, 2019.
- The investigation confirmed that sandbags were damaged more severely than those in the Process Main Building and detected black particles, which were considered activated carbon, in addition to Zeolite. It was also confirmed that the maximum surface dose of sandbags within the investigative scope was 4,000 mSv/h.
- · Based on the investigative results, the dose effect will be assessed.
- ➤ Declining water level in the Unit 1/2 exhaust stack drain sump pit
- The Unit 1/2 exhaust stack drain sump pit is a facility to store rainwater flowing into the Unit 1/2 exhaust stack.

- Accumulated water has been transferred by a pump as required since September 2016.
- On November 26, 2019, a check of water levels in the pit confirmed that the water level had been declining when the transfer pump did not operate since October 12.
- As measures to alleviate any influence based on potential outflow from the pit, the water level of the sump pit was minimized and water-level monitoring was enhanced.
- Based on the dose measurement results near the pit, a decrease in the lower limit of pump suction by replacing the suction pipe will be examined. For similar areas such as a pit and trench, additional measures will also be examined based on the radiation density in contained water.
- Influence on the installation work for the additional Units 1-4 contaminated water transfer equipment by inflow of mortar in the Unit 3 Turbine Building service area
- For contaminated water in buildings flowing into the Unit 3 seawater pipe trench, water transfer, filling and closure
 work was completed in March 2016 except for the connection with the Turbine Building. For the connection, following
 the decline of contaminated water level in buildings, filling started from November 5, 2019.
- For the sump pit in the Unit 3 Turbine Building service area, obstacles were being removed using a muscular robot before installing a new contaminated water transfer pump. On December 3, 2019, however, it was confirmed that filling materials had flown into the area and hardened.
- Measures before installing a contaminated water transfer pump will be decided based on the onsite investigative results.

2. Fuel removal from the spent fuel pools

Work to help remove spent fuel from the pool is progressing steadily while ensuring seismic capacity and safety. The removal of spent fuel from the Unit 4 pool commenced on November 18, 2013 and was completed by December 22, 2014

Main work to help spent fuel removal at Unit 1

- From January 22, 2018, toward fuel removal from the spent fuel pool (SFP), work began to remove rubble on the north side of the operating floor. Once removed, the rubble is stored in solid waste storage facilities or elsewhere depending on the dose level.
- To create an access route for preparatory work to protect the SFP, work to remove four sections of X-braces (one each on the west and south sides and two on the east side, respectively) started from September 19, 2018 and all planned four sections had been removed by December 20.
- From March 18, 2019, the removal of small rubble in the east-side area around the SFP started using pliers and suction equipment, while from July 9, small rubble removal on the south side of the SFP started.
- The well plug, which was considered misaligned from its normal position due to the influence of the hydrogen explosion at the time of the accident, was investigated for the period July 17 August 26, 2019, by taking photos using a camera, measuring the air dose rate and collecting 3D images.
- A prior investigation on September 27, 2019 confirmed the lack of any obstacle which may affect the plan to install
 the cover over the SFP. The investigation also confirmed the absence of any heavy object such as a concrete block,
 which was detected in Unit 3 and the fact that panel- and bar-shaped rubble pieces were scattered on the rack.
- Two methods were examined: (i) installing a cover after rubble removal and (ii) initially installing a large cover over the Reactor Building and then removing rubble inside the cover.
- Following the examination, "the method to initially install a large cover over the Reactor Building and then remove rubble inside the cover" was selected to ensure safer and more secure removal.
- Details of the selected method will be designed and the fuel removal process will be refined.

Main work to help spent fuel removal at Unit 2

- On November 6, 2018, before the investigation toward formulating a work plan to dismantle the Reactor Building rooftop and other tasks, work to move and contain the remaining objects on the operating floor (1st round) was completed.
- On February 1, 2019, an investigation to measure the radiation dose on the floor, walls and ceiling inside the operating floor and confirm the contamination status was completed. After analyzing the investigative results, the "contamination

density distribution" throughout the entire operating floor was obtained, based on which the air dose rate inside the operating floor could be evaluated. A shielding design and measures to prevent radioactive material scattering will be examined.

- From April 8, 2019, work to move and contain the remaining objects on the operating floor (2nd round) started, such as materials and equipment which may hinder installation of the fuel-handling facility and other work. The 2nd round mainly included moving the remaining small objects and placing them in the container. The work also included cleaning the floor to suppress dust scattering and was completed on August 21.
- From September 10, 2019, work to move and contain the remaining objects on the operating floor (3rd round) started, such as materials and equipment which may hinder the installation of the fuel-handling facility and other work. The 3rd round mainly includes moving and containing the remaining large objects as well as transporting containers and remaining objects temporarily stored inside the operating floor outside.
- For fuel removal methods, based on the investigative results inside the operating floor from November 2018 to February 2019, a method to access from a small opening installed on the south side was selected with aspects such as dust management and lower work exposure in mind (the method previously examined had involved fully dismantling the upper part of the building).

Main process to help fuel removal at Unit 3

- From April 15, 2019, the removal of 514 spent fuel assemblies and 52 non-irradiated fuel assemblies (a total of 566 assemblies) stored in the spent fuel pool started. Seven non-irradiated fuel assemblies were then loaded into the transportation cask and transported to the common pool on April 23. The first fuel removal was completed on April 25.
- From July 4, 2019, fuel removal was resumed and up until July 21, 28 of all 566 fuel assemblies had been removed.
- The periodical inspection of the fuel-handling facility, which started on July 24, 2019, was completed on September 2.
 Some defective rotations of the tensile truss and mast were detected during the following adjustment work toward resumption of the fuel removal. In response, parts were replaced and the operation checked to confirm there was no problem.
- Measures were implemented for defects detected during the preparatory work toward resumption of fuel removal and operation was checked using dummy fuel. On December 14, 2019, however, interference of cans inside the transportation cask and dummy fuel was identified. Though the following investigation confirmed slight leaning of the FHM mast, measures, including a review of the procedures, will be implemented to complete fuel removal within FY2020.

> Progress status of dismantling work for the Unit 1/2 exhaust stack

- For the Unit 1/2 exhaust stack, dismantling of the 4th block was completed on December 4, 2019 and the subdrain suspended due to interference of the work was recovered on December 6, 2019. Based on the following review of work to date and refining of the whole process, dismantling is estimated to be completed around early May in 2020 (as spare dates for bad weather, trouble of equipment and other accidents are not considered, the estimated date may change).
- Dismantling of the 5th block started from December 16, 2019 and was completed on December 19.

3. Retrieval of fuel debris

Construction of an access route for the internal investigation of the Unit 1 PCV

- To further enhance dust-density monitoring during the construction of an access route at Unit 1, a dust monitor for the work was installed near the PCV head on November 7, 2019.
- From November 25-28, 2019, work resumed for proven cutting hours to collect more data on dust densities, including that from the newly installed dust monitor. No significant variation was identified in the relevant dust monitor and dust monitors near the site boundary and there was no influence on the outside environment.
- Based on the results, cutting hours will be optimized within the range that has no influence on the surrounding environment and dust reduction methods will also be examined.

Status of examination on fuel debris retrieval

- For fuel debris retrieval from the first implementing unit, methods have been examined; taking the progress status in internal investigations of the Primary Containment Vessel (PCV), the status of improvement in the work environment and other factors into consideration.
- The characteristics of the debris acquired by the contact investigation in February 2019 and, the status of improvement in the environment on the 1st floor of the Reactor Building for access to PCV and the engineering works with these results taken into consideration and Unit 2 was evaluated that it is suitable for the first implementing unit for fuel debris retrieval.
- As the method, to determine, a trial retrieval using a robot arm will begin. After verifying and checking this retrieval method, the scale will be gradually expanded using equipment with the same mechanism.

4. Plans to store, process and dispose of solid waste and decommission of reactor facilities

Promoting efforts to reduce and store waste generated appropriately and R&D to facilitate adequate and safe storage, processing and disposal of radioactive waste

Management status of the rubble and trimmed trees

• As of the end of November 2019, the total storage volume of the concrete and metal rubble was approx. 281,400 m³ (+2,600 m³ compared to at the end of October with an area-occupation rate of 70%). The total storage volume of trimmed trees was approx. 134,100 m³ (slight increase, with an area-occupation rate of 76%). The total storage volume of used protective clothing was approx. 49,900 m³ (-2,700 m³, with an area-occupation rate of 73%). The increase in rubble was mainly attributable to tank-related construction, while the decrease in used protective clothing was attributable to the incinerator operation.

Management status of secondary waste from water treatment

As of December 5, 2019, the total storage volume of waste sludge was 597 m³ (area-occupation rate: 85%), while that of concentrated waste fluid was 9,345 m³ (area-occupation rate: 91%). The total number of stored spent vessels, High-Integrity Containers (HICs) for multi-nuclide removal equipment and other vessels, was 4,576 (area-occupation rate: 72%).

5. Reduction in radiation dose and mitigation of contamination

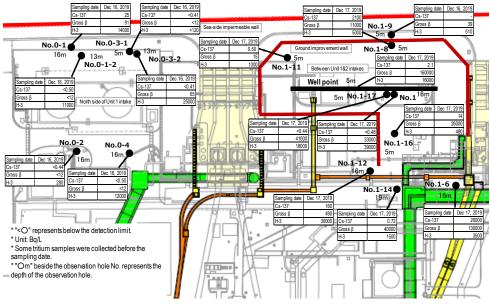
Effective dose-reduction at site boundaries and purification of port water to mitigate the impact of radiation on the external environment

Status of groundwater and seawater on the east side of Turbine Building Units 1-4

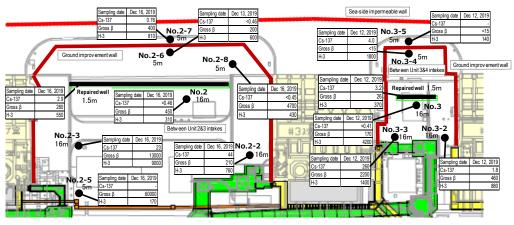
- At No. 1-6, the H-3 density had been declining from around 6,000 Bq/L to 1,000 Bq/L since October 2019 and then increasing. It currently stands at around 3,500 Bq/L.
- At No. 1-9, the density of gross β radioactive materials has been repeatedly increasing and declining from around 20 Bg/L since April 2019 and currently stands at around 40 Bg/L.
- At No. 1-14, the H-3 density has been repeatedly increasing and declining from around 1,300 Bq/L since July 2019 and currently stands at around 1,500 Bq/L. Since August 15, 2013, pumping of groundwater continued (at the well point between the Unit 1 and 2 intakes: August 15, 2013 October 13, 2015 and from October 24; at the repaired well: October 14-23, 2015).
- At No. 2-3, the H-3 density had been declining from around 6,000 Bq/L since August 2019, then increasing and currently stands at around 9,000 Bq/L. The density of gross β radioactive materials at the same point had been declining from around 14,000 Bq/L to around 5,000 Bq/L since August 2019, then increasing and currently stands at around 13,000 Bq/L.
- At No. 2-5, the H-3 density had been declining from around 2,300 Bq/L to less than 120 Bq/L since June 2019, then repeatedly increasing and declining and currently stands at less than 170 Bq/L. The density of gross β radioactive materials at the same point had been declining from around 65,000 Bq/L to around 500 Bq/L since September 2019, then increasing and currently stands at around 60,000 Bq/L.
- At No. 2-6, the density of gross β radioactive materials had been increasing from around 100 Bq/L since May 2019

and currently stands at around 200 Bq/L. Since December 18, 2013, pumping of groundwater continued (at the well point between the Unit 2 and 3 intakes: December 18, 2013 - October 13, 2015; at the repaired well: from October 14, 2015).

- The densities of radioactive materials in drainage channels have remained constant, despite increasing during rainfall.
- In the Units 1-4 intake open channel area, densities of radioactive materials in seawater have remained below the legal discharge limit, while increasing in Cs-137 and Sr-90 below the legal discharge limit during rainfall. They have also been declining following the completed installation and the connection of steel pipe sheet piles for the sea-side impermeable walls. The density of Cs-137 has remained slightly higher in front of the south side impermeable walls and slightly lower on the north side of the east breakwater since March 20, 2019, when the silt fence was transferred to the center of the open channel due to mega float-related construction.
- In the area within the port, densities of radioactive materials in seawater have remained below the legal discharge limit, while increasing in Cs-137 and Sr-90 below the legal discharge limit during rainfall. They have remained below the level of those in the Units 1-4 intake open channel area and been declining following the completed installation and connection of steel pipe sheet piles for the sea-side impermeable walls.
- In the area outside the port, regarding the densities of radioactive materials in seawater, those of Cs-137 and Sr-90
 declined and remained low after steel pipe sheet piles for the sea-side impermeable walls were installed and
 connected.



<Unit 1 intake north side, between Unit 1 and 2 intakes>



<Between Unit 2 and 3 intakes, between Unit 3 and 4 intakes>

Figure 5: Groundwater density on the Turbine Building east side

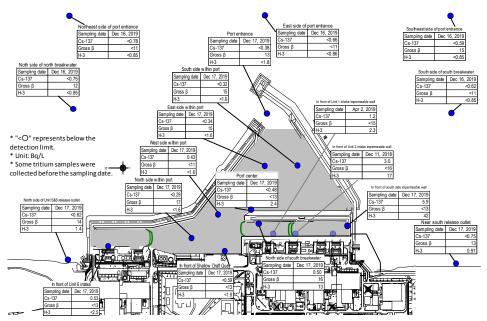


Figure 6: Seawater density around the port

6. Outlook of the number of staff required and efforts to improve the labor environment and conditions

Securing appropriate staff long-term while thoroughly implementing workers' exposure dose control. Improving the work environment and labor conditions continuously based on an understanding of workers' on-site needs

> Staff management

- The monthly average total of personnel registered for at least one day per month to work on site during the past quarter from August to October 2019 was approx. 8,900 (TEPCO and partner company workers), which exceeded the monthly average number of actual workers (approx. 6,600). Accordingly, sufficient personnel are registered to work on site.
- It was confirmed with the prime contractors that the estimated manpower necessary for the work in January 2020 (approx. 3,900 per day: TEPCO and partner company workers) would be secured at present. The average numbers of workers per day per month (actual values) were maintained, with approx. 3,400 to 5,600 since FY2017 (see Figure 7).
- The number of workers from within Fukushima Prefecture increased. The local employment ratio (TEPCO and partner company workers) as of November 2019 has remained constant at around 60%.
- The monthly average exposure dose of workers remained at approx. approx. 0.39, 0.36 and 0.32 mSv/month during FY2016, FY2017 and FY2018 respectively. (Reference: Annual average exposure dose 20 mSv/year ≒ 1.7 mSv/month)
- For most workers, the exposure dose was sufficiently within the limit and allowed them to continue engaging in radiation work.

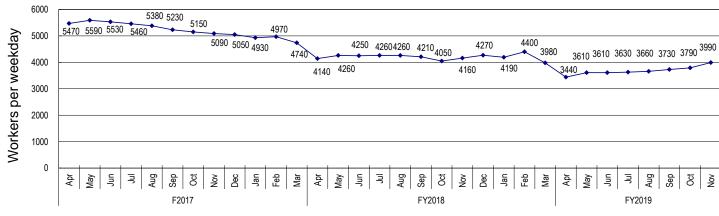
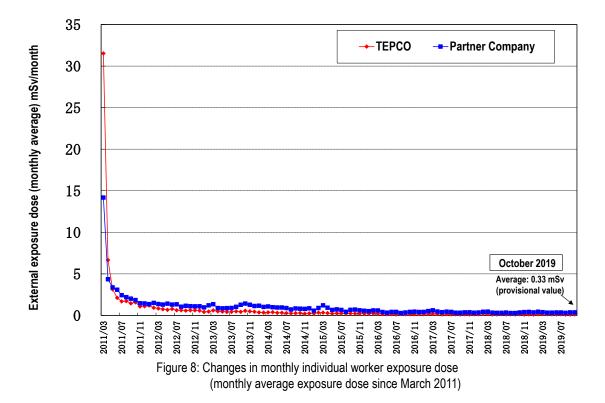


Figure 7: Changes in the average number of workers per weekday for each month since FY2017 (actual values)



➤ Measures to prevent infection and expansion of influenza and norovirus

• Since November, measures for influenza and norovirus have been implemented, including free influenza vaccinations (subsidized by TEPCO HD) in the Fukushima Daiichi Nuclear Power Station (from November 13 to December 13, 2019) for partner company workers. Free influenza vaccinations are also provided at medical clinics around the site (from December 2, 2019 to January 30, 2020). As of December 16, 2019, a total of 5,091 workers had been vaccinated. In addition, a comprehensive range of other measures is also being implemented, including daily actions to prevent infection and expansion (measuring body temperature, health checks and monitoring infection status) and response after detecting possible infections (swift exit of possible patients and control of entry, mandatory wearing of masks in working spaces, etc.).

Status of influenza and norovirus cases

 Until the 50th week of 2019 (December 9-15, 2019), 63 influenza infections and three norovirus infections were recorded. The totals for the same period for the previous season showed two cases of influenza and four norovirus infections.

7. Status of Units 5 and 6

> Status of spent fuel storage in Units 5 and 6

- Regarding Unit 5, fuel removal from the reactor was completed in June 2015. A total of 1,374 spent and 168 non-irradiated fuel assemblies, respectively, were stored in the spent fuel pool (storage capacity: 1,590 assemblies).
- Regarding Unit 6, fuel removal from the reactor was completed in November 2013. A total of 1,456 spent and 198 non-irradiated fuel assemblies (180 of which transferred from the Unit 4 spent fuel pool) are stored in the spent fuel pool (storage capacity: 1,654), while 230 non-irradiated fuel assemblies are stored in the storage facility of non-irradiated fuel assemblies (storage capacity: 230).

Status of contaminated water treatment in Units 5 and 6

• Contaminated water in Units 5 and 6 is transferred from Unit 6 Turbine Building to the outdoor tanks and sprinkled after undergoing oil separation and RO treatment and confirming the density of the radioactive materials.

Status of seawater monitoring within the port (comparison between the highest values in 2013 and the latest values)

"The highest value" → "the latest value (sampled during December 9-17)"; unit (Bg/L); ND represents a value below the detection limit Source: TEPCO website Analysis results on nuclides of radioactive materials around Fukushima Daiichi Nuclear Cesium-134: 3.3 (2013/10/17) \rightarrow ND(0.28) Below 1/10 Power Station http://www.tepco.co.jp/nu/fukushima-np/f1/smp/index-j.html Cesium-137: 9.0 (2013/10/17) \rightarrow ND(0.34) Below 1/20

Tritium:

Silt fence

Sea side impermeable wall

 $(2013/8/19) \rightarrow 15$ Below 1/4 $(2013/8/19) \rightarrow ND(1.6)$ Below 1/40 Cesium-134: ND(0.60) Cesium-137: ND(0.48) Gross β: ND(13)

Cesium-137: 7.3 (2013/10/11) \rightarrow ND(0.38)Below 1/10 Gross β:

Cesium-134: 3.3 (2013/12/24) \rightarrow ND(0.51) Below 1/6

Cesium-134: 4.4 (2013/12/24) \rightarrow ND(0.36) Below 1/10 $(2013/12/24) \rightarrow 0.43$

Below 1/20

2.4

[Port entrance]

 $(2013/8/19) \rightarrow 13$ Below 1/5 Tritium: $(2013/8/19) \rightarrow ND(1.8)$ Below 1/30

Gross β: $(2013/7/4) \rightarrow ND(11)$ Below 1/5 Tritium: $(2013/8/19) \rightarrow ND(1.6)$ Below 1/30

Gross β:

Cesium-134: 3.5 (2013/10/17) \rightarrow ND(0.28) Below 1/10 Cesium-137: 7.8 (2013/10/17) \rightarrow ND(0.32) Below 1/20 $(2013/8/19) \rightarrow 15$ Below 1/5

Cesium-134: 5.0 (2013/12/2) \rightarrow ND(0.27) Below 1/10

South side

in the port

[Port center]

Tritium:

Cesium-137: 8.4 (2013/12/2) \rightarrow ND(0.29) Gross β: $(2013/8/19) \rightarrow 17$

Below 1/20 Below 1/4

Cesium-134: 32 (2013/10/11) \rightarrow ND(0.44) Below 1/70

60 (2013/8/19) \rightarrow ND(1.6) Below 1/30

Tritium: $(2013/8/19) \rightarrow ND(1.6)$

 $(2013/8/19) \rightarrow ND(13)$

 $(2013/8/19) \rightarrow ND(2.5)$

WHO

Below 1/30

[East side in the port]

Cesium-137: 73 (2013/10/11) \rightarrow 0.50 Below 1/100 Gross β: Tritium:

320 (2013/ 8/12) → 16 510 (2013/ 9/ 2) → 13

From February 11, 2017, the location of the sampling point was shifted

approx. 50 m south of the previous point due to the location shift of the silt

Cesium-134: 2.8 (2013/12/2) \rightarrow ND(0.48) Cesium-137: 5.8 (2013/12/2) \rightarrow 0.53 Gross β: Tritium:

Tritium

Gross β:

Tritium:

Cesium-137: 10

Below 1/10

Cesium-134:

Cesium-137:

Below 1/3 Below 1/9

Below 1/5

[West side in the port]

Cesium-134: ND(0.50) Cesium-137: 5.9 ND(13)

42

*1: Monitoring commenced in or after March

2014. Monitoring inside the sea-side

impermeable walls was finished because

Gross B: Tritium:

Legal **Guidelines for** discharge Drinking limit **Water Qualit** 10 Cesium-134 60 10 90 Cesium-137 Strontium-90 (strongly 30 10 correlăte with Gross β) 60.000 10.000

[North side in the port]

In front of shallow draft quay] [In front of Unit 6 intake]

Unit 2

of the landfill. *2: For the point, monitoring was finished from December 12, 2018 due to preparatory work for transfer of mega float.

3: For the point, monitoring point was moved from February 6, 2019 due to preparatory work for transfer of mega

For the point, monitoring was finished from April 3, 2019 due to preparatory work for transfer of mega float.

(approx. 12 Bg/L). They also include the contribution of yttrium

Unit 3

Note: The gross β measurement values include natural potassium 40

90, which radioactively balance strontium 90.

Unit 4

Summary of TEPCO data as of December 18, 2019

Gross β: $(2013/7/3) \rightarrow ND(13)$ Below 1/3 Tritium: 340 $(2013/6/26) \rightarrow ND(1.8)$ Below 1/100

 $5.3 (2013/8/5) \rightarrow ND(0.53)$ Below 1/10

8.6 (2013/8/ 5) \rightarrow ND(0.59) Below 1/10

1/2

Below 1/20

Below 1/30

Status of seawater monitoring around outside of the port (comparison between the highest values in 2013 and the latest values)

(The latest values sampled during December 9-17)

Legal discharge for Drinking limit **Water Quality** Cesium-134 60 10 10 90 Cesium-137 Strontium-90 (strongly correlate with 30 10 Gross β) 60,000 10,000 Tritium

Unit (Bg/L); ND represents a value below the detection limit; values in () represent the detection limit; ND (2013) represents ND throughout 2013

Northeast side of port entrance(offshore 1km) \(\) [East side of port entrance (offshore 1km)]

[Southeast side of port entrance(offshore 1km)]

Cesium-134: ND (2013) \rightarrow ND (0.44) Cesium-137: $ND (2013) \rightarrow ND (0.78)$ Gross β: $ND (2013) \rightarrow ND (11)$ Tritium: $ND (2013) \rightarrow ND (0.85)$ Cesium-134: ND (2013) \rightarrow ND (0.61) Cesium-137: 1.6 (2013/10/18) \rightarrow ND (0.66) Below 1/2

[Port entrance]

Gross β: ND (2013) \rightarrow ND (11) Tritium: $6.4 (2013/10/18) \rightarrow ND (0.86)$ Below 1/7

Cesium-137: ND (2013) \rightarrow ND (0.59)

Cesium-134: ND (2013) \rightarrow ND (0.68)

Gross β: ND $(2013) \rightarrow 15$

Tritium: $ND (2013) \rightarrow ND (0.85)$

Cesium-134: ND (2013) \rightarrow ND (0.74) Cesium-137: ND (2013) \rightarrow ND (0.75) Gross β: \rightarrow 12 ND (2013)

Tritium: 4.7 (2013/8/18) \rightarrow ND (0.85) Below 1/5

[South side of south breakwater(offshore 0.5km)]

North side of north breakwater(offshore 0.5km)

Cesium-134: 3.3 (2013/12/24) \rightarrow ND (0.51) Below 1/6 [North side of Unit 5 and 6 release outlet] Cesium-137: 7.3 (2013/10/11) \rightarrow ND (0.38) Below 1/10

Cesium-134: 1.8 (2013/ 6/21) \rightarrow ND (0.59) Below 1/3

Gross β: Tritium:

 $(2013/8/19) \rightarrow 13$ 68 $(2013/8/19) \rightarrow ND (1.8)$

Below 1/5 Below 1/30

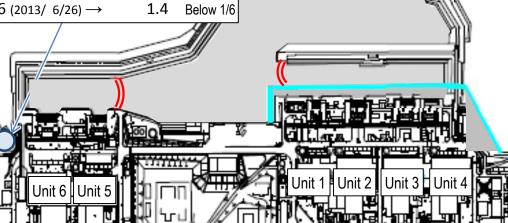
Cesium-134: ND (2013) \rightarrow ND (0.79) Cesium-137: ND (2013) \rightarrow ND (0.62) Gross β: $ND (2013) \rightarrow ND (11)$ Tritium: $ND (2013) \rightarrow ND (0.85)$

Cesium-137: 4.5 (2013/ 3/17) \rightarrow ND (0.69) Below 1/6 Gross β: **12** (2013/12/23) → 14 Tritium:

 $8.6 (2013/6/26) \rightarrow$ 1.4

Note: The gross β measurement values include natural potassium 40 (approx. 12 Bg/L).

They also include the contribution of yttrium 90, which radioactively balance strontium 90.



Cesium-137: 3.0 (2013/ 7/15) \rightarrow ND (0.75) Below 1/4 Gross β: 15 $(2013/12/23) \rightarrow 13$ Tritium: $1.9 (2013/11/25) \rightarrow$ 1.3 [Near south release outlet]

Sea side impermeable wall Silt fence

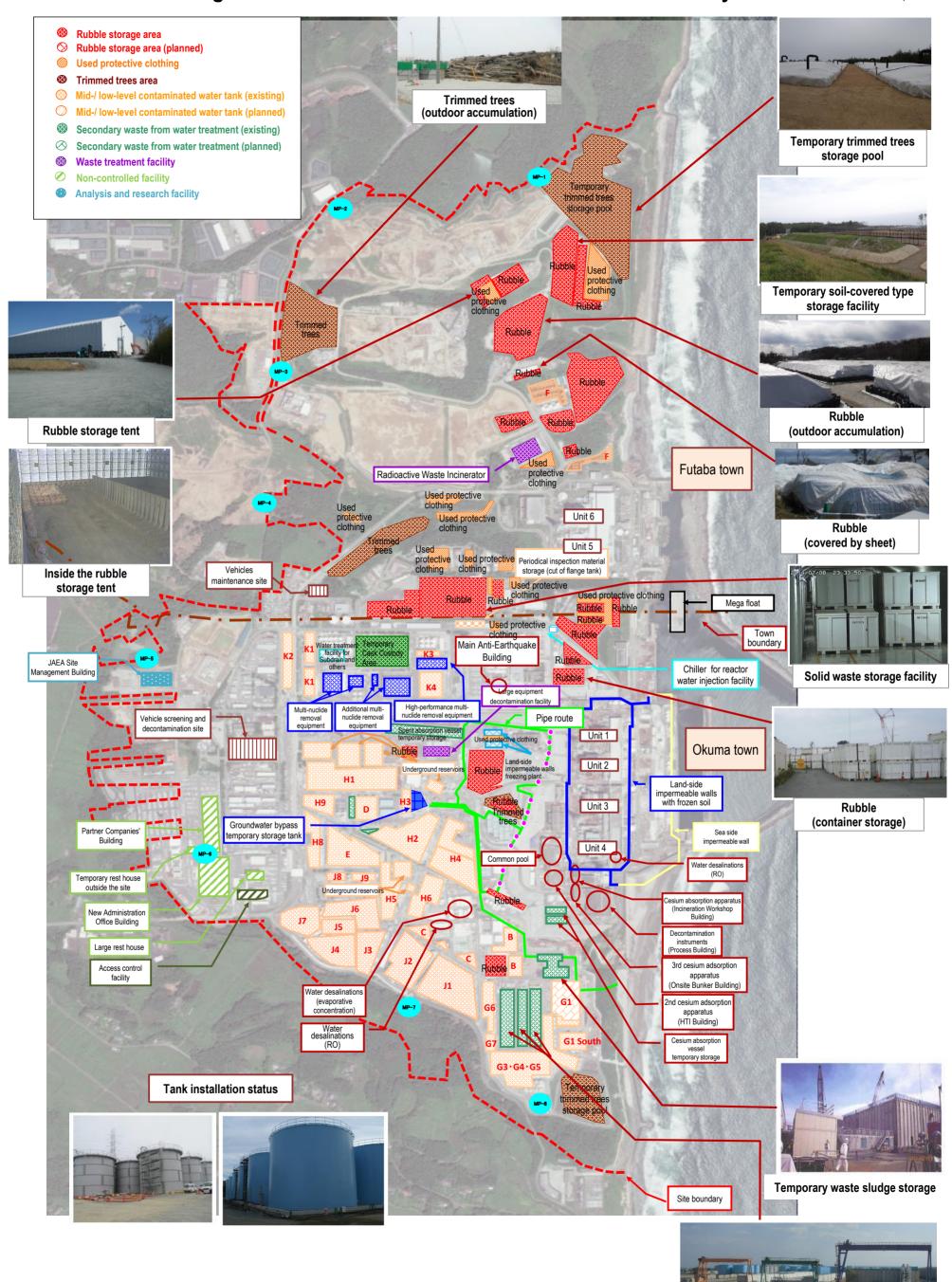
Cesium-134: ND (2013)

Note: Because safety of the sampling points was unassured due to the influence of Typhoon No. 10 in 2016, samples were taken from approx. 330 m south of the Unit 1-4 release outlet. Samples were also taken from a point approx. 280m south from the same release outlet from January 27, 2017 and approx. 320m from March 23, 2018

Summary of TEPCO data as of December 18, 2019

 \rightarrow ND (0.63)

TEPCO Holdings Fukushima Daiichi Nuclear Power Station Site Layout



Spent adsorption vessel temporary storage facility

Provided by Japan Space Imaging, photo taken on June 14, 2018 Product(C) [2018] DigitalGlobe, Inc.

Progress toward decommissioning: Fuel removal from the spent fuel pool (SFP)

Immediate target

Commence fuel removal from the Unit 1-3 Spent Fuel Pools

December 19, 2019 Secretariat of the Team for Countermeasures for Decommissioning and Contaminated Water Treatment

Unit 1

Toward fuel removal from the Unit 1 spent fuel pool, investigations have been implemented to ascertain the conditions of the fallen roof on the south side and the contamination of the well plug. Based on the results of these investigations, "the method to initially install a large cover over the Reactor Building and then remove rubble inside the cover" was selected to ensure a safer and more secure removal. Details of the selected method will be designed and the process of fuel removal will be refined.

<Reference> Progress to date

Rubble removal on the north side of the operating floor started from January 2018 and has been implemented sequentially. In July and August 2019, the well plug, which was misaligned from its normal position, was investigated and in August and September, the conditions of the overhead crane were checked. Based on the results of these investigations, as the removal requires more careful work taking dust scattering into consideration, two methods were examined: installing a cover after rubble removal and initially installing a large cover over the Reactor Building and then removing rubble inside the cover.



Rubble removal (image)

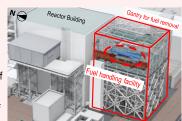


Fuel removal (image)

Unit 2

Toward fuel removal from the Unit 2 spent fuel pool, based on findings from internal operating floor investigations from November 2018 to February 2019, instead of fully dismantling the upper part of the building, the decision was made to install a small opening on the south side and use a boom crane. The changed method will be established and the fuel removal process refined.

<Reference> Progress to date Previously, potential to recover the existing overhead crane and the fuel handling machine was examined. However, the high radiation dose inside the operating floor meant the decision was taken to dismantle the upper part of the building in November 2015. Findings from internal investigations of the operating floor from November 2018 to February 2019 underlined the potential to conduct limited work there and the means of accessing from the south side had been



Overview of fuel removal (bird's-eye view)

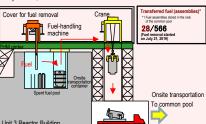
Unit 3

Prior to the installation of a cover for fuel removal, removal of large rubble from the spent fuel pool was completed in November 2015. To ensure safe and steady fuel removal, training of remote control was conducted at the factory using the actual fuel-handling machine which will be installed on site (February – December 2015). Measures to reduce dose on the Reactor Building top floor (decontamination, shields) were completed in December 2016. Installation of a cover for fuel removal and a fuel-handling machine is underway from January 2017. Installation of the fuel removal cover was completed on February 23, 2018.

Toward fuel removal, the rubble retrieval training inside the pool, which was scheduled in conjunction with fuel removal training, started from March 15, 2019, and started fuel removal from April 15, 2019.







Installation of dome roof (February 21, 2019) Overview of the fuel-handling facility inside the cover



Fuel removal status (April 15, 2019)

Unit 4

examined.

In the Mid- and Long-Term Roadmap, the target of Phase 1 involved commencing fuel removal from inside the spent fuel pool (SFP) of the 1st Unit within two years of completion of Step 2 (by December 2013). On November 18, 2013, fuel removal from Unit 4, or the 1st Unit, commenced and Phase 2 of the roadmap started

On November 5, 2014, within a year of commencing work to fuel removal, all 1,331 spent fuel assemblies in the pool had been transferred. The transfer of the



Fuel removal status

remaining non-irradiated fuel assemblies to the Unit 6 SFP was completed on December 22. 2014. (2 of the non-irradiated fuel assemblies were removed in advance in July 2012 for fuel checks)

This marks the completion of fuel removal from the Unit 4 Reactor Building. Based on this experience, fuel assemblies will be removed from Unit 1-3 pools.

* A part of the photo is corrected because it includes sensitive information related to

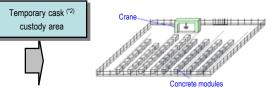
Common pool

pit Storage area

An open space will be maintained in the common pool (Transfer to the temporary cask custody area)

Progress to date

- The common pool has been restored to a condition allowing it to re-accommodate fuel to be handled (November 2012)
- · Loading of spent fuel stored in the common pool to dry casks commenced (June 2013)
- Fuel removal from the Unit 4 spent fuel pool began to be received (November 2013 - November 2014)
- Fuel removal from the Unit 3 spent fuel pool began to be received (from April 2019)



Spent fuel is accepted from the common pool

Operation commenced on April 12, 2013; from the cask-storage building, transfer of 9 existing dry casks completed (May 21, 2013); fuel stored in the common pool sequentially transferred

(*1) Operating floor: During regular inspection, the roof over the reactor is opened while on the operating floor, fuel inside the core is replaced and the core internals are inspected. (*2) Cask: Transportation container for samples

and equipment, including radioactive materials.

Secretariat of the Team for Countermeasures for Decommissioning and Contaminated Water Treatment

Immediate target

Identify the plant status and commence R&D and decontamination toward fuel debris retrieval

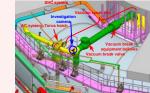
Investigation into TIP Room of the Unit 1 Reactor Building

- To improve the environment for future investigations inside the PCV, etc., an investigation was conducted from September 24 to October 2, 2015 at the TIP Room. (*1). (Due to high dose around the entrance in to the TIP Room, the investigation of dose rate and contamination distribution was conducted through a hole drilled from the walkway of the Turbine Building. where the dose was low)
- The investigative results identified high dose at X-31 to 33 penetrations(*2) (instrumentation penetration) and low dose at
- · As it was confirmed that work inside the TIP room would be available, the next step will include identification of obstacles which will interfere the work inside the TIP Room and formulation of a plan for dose reduction.

Investigation in the leak point detected in the upper part of

the Unit 1 Suppression Chamber (S/C^(*3))
Investigation in the leak point detected in the upper part of Unit 1 S/C from May 27, 2014 from one expansion joint cover among the lines installed there. As no leakage was identified from other parts, specific methods will be examined to halt the flow of water and repair the PCV.





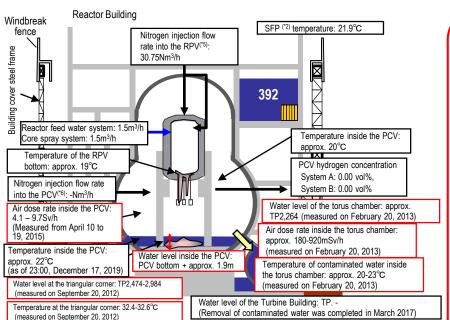
Leak point

Image of the S/C upper part investigation

Unit 1

Air dose rate inside the Reactor Building:

Max. 5,150mSv/h (1F southeast area) (measured on July 4, 2012)



	^a Indices related to the plant are values as of 11:00, December 18, 2019				
	Investigations inside PCV	1st (Oct 2012)	- Acquiring images - Measuring air temperature and dose rate - Measuring water level and temperature - Sampling contaminated water - Installing permanent monitoring instrumentation	l	
		2nd (Apr 2015)	Confirming the status of PCV 1st floor - Acquiring images - Measuring air temperature and dose rate - Replacing permanent monitoring instrumentation	\	
		3 rd (Mar 2017)	Confirming the status of PCV 1st basement floor - Acquiring images - Measuring and dose rate - Sampling deposit - Replacing permanent monitoring instrumentation		
	Leakage points from	PCV vent pipe vacuum break line bellows (identified in May 2014) Sand cushion drain line (identified in November 2013)			

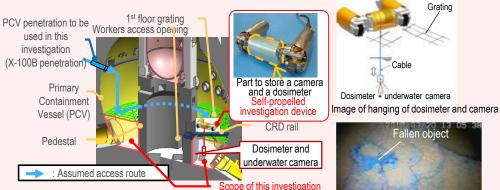
Status of investigation inside the PCV

Prior to fuel debris retrieval, an investigation inside the PCV will be conducted to inspect the status there including the location of fuel debris.

[Investigative outline]

- In April 2015, a device, which entered the inside of the PCV through a narrow access opening (bore: φ 100 mm). collected information such as images and airborne dose inside the PCV 1st floor.
- In March 2017, the investigation using a self-propelled investigation device, conducted to inspect the spreading of debris to the basement floor outside the pedestal, took images of the PCV bottom status for the first time. The status inside the PCV will continue to be examined based on the collected image and dose data.

(the 3rd time)



<Image of investigation inside the PCV>

Image near the bottom

Capturing the location of fuel debris inside the reactor by measurement using muons

Period	Evaluation results	
Feb - May 2015	Confirmed that there was no large fuel in the reactor core.	

- (*1) TIP (Traversing In-core Probe)
- (*2) Penetration: Through-hole of the PCV
- (*3) S/C (Suppression Chamber): Suppression pool, used as the water source for the emergent core cooling system.

Grating

- (*4) SFP (Spent Fuel Pool):
- (*5) RPV (Reactor Pressure Vessel) (*6) PCV (Primary Containment Vessel)
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December 19, 2019

Identify the plant status and commence R&D and decontamination toward fuel debris retrieval

Secretariat of the Team for Countermeasures for Decommissioning and Contaminated Water Treatment

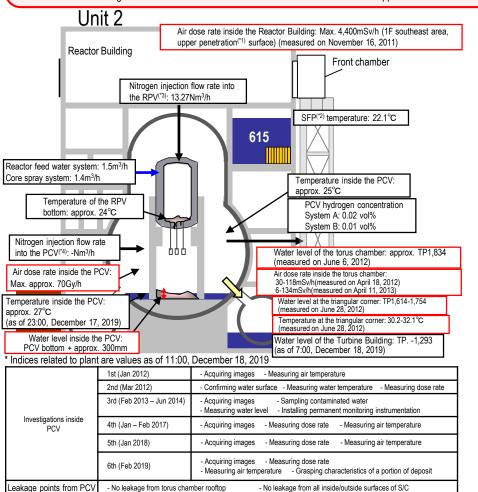
Installation of an RPV thermometer and permanent PCV supervisory instrumentation

(1) Replacement of the RPV thermometer

Immediate

target

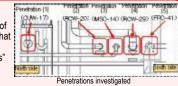
- As the thermometer installed at the Unit 2 RPV bottom after the earthquake had broken in February 2014, it was excluded from the monitoring thermometers.
- In April 2014, removal of the broken thermometer failed and was suspended. Rust-stripping chemicals were injected and the
 broken thermometer was removed in January 2015. A new thermometer was reinstalled in March. The thermometer has been
 used as a part of permanent supervisory instrumentation since April.
- (2) Reinstallation of the PCV thermometer and water-level gauge
- Some of the permanent supervisory instrumentation for PCV could not be installed in the planned locations due to interference
 with existing grating (August 2013). The instrumentation was removed in May 2014 and new instruments were reinstalled in
 June 2014. The trend of added instrumentation will be monitored for approx. one month to evaluate its validity.
- The measurement during the installation confirmed that the water level inside the PCV was approx. 300mm from the bottom.



Investigative results on torus chamber walls

 The torus chamber walls were investigated (on the north side of the east-side walls) using equipment specially developed for that purpose (a swimming robot and a floor traveling robot).

- At the east-side wall pipe penetrations (five points), "the status" and "existence of flow" were checked.
- A demonstration using the above two types of underwater wall investigative equipment showed how the equipment could check the status of penetration.
- Regarding Penetrations 1 5, the results of checking the sprayed tracer (*5) by camera showed no flow around the penetrations. (investigation by the swimming robot)
- Regarding Penetration 3, a sonar check showed no flow around the penetrations. (investigation by the floor traveling robot)



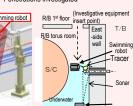
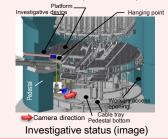


Image of the torus chamber east-side cross-sectional investigation

Status of investigation inside the PCV

Prior to fuel debris retrieval, an investigation inside the PCV will be conducted to inspect the status there including the location of fuel debris. [Investigative outline]

- Investigative devices such as a robot will be injected from Unit 2 X-6 penetration⁽¹⁾ and access the inside of the pedestal using the CRD rail. [Progress status]
- On January 26 and 30, 2017, a camera was inserted from the PCV penetration to inspect the status of the CRD replacement rail
 on which the robot will travel. On February 9, deposit on the access route of the self-propelled investigative device was removed
 and on February 16, the inside of the PCV was investigated using the device.
- The results of this series of investigations confirmed fallen and deformed gratings and a quantity of deposit inside the pedestal.
- On January 19, 2018, the status below the platform inside the pedestal was investigated using an investigative device with a
 hanging mechanism. From the analytical results of images obtained in the investigation, deposits probably including fuel debris
 were found at the bottom of the pedestal. In addition, multiple parts higher than the surrounding deposits were also detected. We
 presumed that there were multiple routes of fuel debris falling. Obtained data were processed in panoramic image visualization
 to accourie clearer images.
- On February 13, 2019, an investigation touching the deposits at the bottom of the pedestal and on the platform was conducted
 and confirmed that the pebble-shaped deposits, etc. could be moved and that hard rock-like deposits that could not be gripped
 may exist.
- In addition, images, etc. would help determine the contour and size of the deposits could be collected by moving the
 investigative unit closer to the deposits than the previous investigation.





Bottom of the pedestal (after being processed in panoramic image visualization)

Capturing the location of fuel debris inside the reactor by measurement using muons

Period	Evaluation results	
Mar – Jul 2016	Confirmed the existence of high-density materials, which was considered as fuel debris, at the bottom of RPV, and in the lower part and the outer periphery of the reactor core. It was assumed that a large part of fuel debris existed at the bottom of RPV.	

(*1) Penetration: Through-hole of the PCV (*2) SFP (Spent Fuel Pool) (*3) RPV (Reactor Pressure Vessel) (*5) Tracer: Material used to trace the fluid flow. Clay particles

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Immediate target

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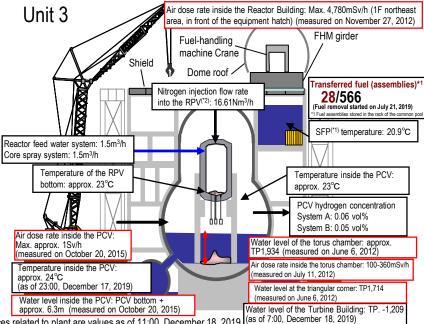
Water flow was detected from the Main Steam Isolation Valve* room

On January 18, 2014, a flow of water from around the door of the Steam Isolation Valve room in the Reactor Building Unit 3 1st floor northeast area to the nearby floor drain funnel (drain outlet) was detected. As the drain outlet connects with the underground part of the Reactor Building, there is no possibility of outflow from the building.

From April 23, 2014, image data has been acquired by camera and the radiation dose measured via pipes for measurement instrumentation, which connect the air-conditioning room on the Reactor Building 2nd floor with the Main Steam Isolation Valve Room on the 1st floor. On May 15, 2014, water flow from the expansion joint of one Main Steam Line was detected.

This is the first leak from PCV detected in the Unit 3. Based on the images collected in this investigation, the leak volume will be estimated and the need for additional investigations will be examined. The investigative results will also be utilized to examine water stoppage and PCV repair methods.

* Main Steam Isolation Valve: A valve to shut off the steam generated from the Reactor in an emergency



indices related to plant are values as of 11.00, December 16, 2019				
Investigations inside PCV	1st (Oct – Dec 2015)	- Acquiring images - Measuring air temperature and dose rate - Measuring water level and temperature - Sampling contaminated water - Installing permanent monitoring instrumentation (December 2015)		
	2nd (Jul 2017)	- Acquiring images - Installing permanent monitoring instrumentation (August 2017)		
Leakage points from PCV	- Main steam pipe bellows (identified in May 2014)			

Investigative results into the Unit 3 PCV equipment hatch using a small investigation device

As part of the investigation into the PCV to facilitate fuel debris retrieval, the status around the Unit 3 PCV equipment hatch was investigated using a small self-traveling investigation device on

November 26, 2015.

• Given blots such as rust identified below the

water level inside the PCV, there may be a leakage from the seal to the extent of bleeding.

Methods to investigate and repair the parts, including other PCV penetrations with a similar structure, will be considered.



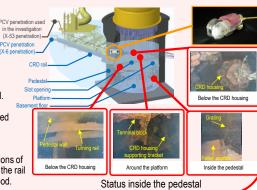
Investigation inside the PCV

Prior to fuel debris retrieval, the inside of the Primary Containment Vessel (PCV) was investigated to identify the status there including the location of the fuel debris.

[Investigative outline]

- The status of X-53 penetration^(*4), which may be under the water and which is scheduled for use to investigate the inside of the PCV, was investigated using remote-controlled ultrasonic test equipment. The results showed that the penetration was not under the water (October 22-24, 2014).
- For the purpose of confirming the status inside the PCV, an investigation device was inserted into the PCV from X-53 penetration on October 20 and 22, 2015 to obtain images, data of dose and temperature and sample contaminated water. No damage was identified on the structure and walls inside the PCV and the water level was almost identical with the estimated value. In addition, the dose inside the PCV was confirmed to be lower than in other Units.

 PCV penetration used in the investigation (X-53 penetration)
 PCV penetration (X-65 penetration)
 PCV penetration (X-65
- In July 2017, the inside of the PCV was investigated using the underwater ROV (remotely operated underwater vehicle) to inspect the inside of the pedestal.
- Analysis of image data obtained in the investigation identified damage to multiple structures and the supposed core internals. Consideration about fuel removal based on the obtained information will continue.
- Videos obtained in the investigation were reproduced in 3D. Based on the reproduced images, the relative positions of the structures, such as the rotating platform slipping off the rail with a portion buried in deposits, were visually understood.



Capturing the location of fuel debris inside the reactor by measurement using muons

Period	Evaluation results
May – Sep 2017	The evaluation confirmed that no large lump existed in the core area where fuel had been placed and that part of the fuel debris potentially existed at the bottom of the RPV.

(*1) SFP (Spent Fuel Pool) (*2) RPV (Reactor Pressure Vessel) (*3) PCV (Primary Containment Vessel) (*4) Penetration: Through-hole of the PCV

Immediate target

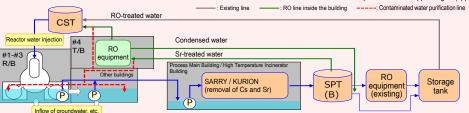
Stably continue reactor cooling and contaminated water treatment, and improve reliability

Work to improve the reliability of the circulation water injection cooling system and pipes to transfer contaminated water.

- Operation of the reactor water injection system using Unit 3 Condensate Storage Tank (CST) as a water source commenced (from July 5, 2013). Compared to the previous systems, the reliability of the reactor water injection system was enhanced, e.g. by increasing the amount of water-source storage and enhancing durability.
 To reduce the risk of contaminated-water leakage, the circulation loop was shortened by installing a reverse osmosis (RO) device in the Unit 4 Turbine Building within the circulation
- To reduce the risk of contaminated-water leakage, the circulation loop was shortened by installing a reverse osmosis (RO) device in the Unit 4 Turbine Building within the circulation loop, comprising the transfer of contaminated water, water treatment and injection into the reactors. Operation of the installed RO device started from October 20. Installation of the new RO device inside the building shortened the circulation loop from approx. 3 to 0.8 km.
- To accelerate efforts to reduce the radiation density in contaminated water inside the buildings, circulating purification of contaminated water inside the buildings stared on the Unit 3 and 4 side on February 22 and on the Unit 1 and 2 side on April 11.
- For circulating purification, a new pipe (contaminated water purification line) divided from the water treatment equipment outlet line was installed to transfer water purified at the water treatment equipment to the Unit 1 Reactor Building and the Unit 2-4 Turbine Buildings.
- The risks of contaminated water inside the buildings will continue to be reduced in addition to reduction of its storage.

* The entire length of contaminated water transfer pipes is approx. 2.1km, including the transfer line of surplus water to the upper heights (approx. 1.3km).

Storage tank



Storage tank (treated water) Buffer tank (RO concentrated Multi-nuclide Reliability increase salt water) removal equipment, etc Reactor Building Mobile strontiummoval equipment Condensate Storage tank Reactor water Salt treatment Turbine injection pump (RO Building membrane) Storage tank (strontium-treated Contaminated water, etc.) water treatment (Kurion/Sarry) Facilities improvement Legend Estimated leak route 6 Paved with asphalt 3 Groundwater bypass Rain Cs/Sr removal desalination Reactor building 7 Ground Groundwater level 4 Sub-drain improvement by 4 Sub-drain Turbine sodium silicate building Upper permeable layer Low-permeable layer Pumping well Lower permeable layer Well point Low-permeable laver

SLand-side impermeable wall

(5)Land-side impermeable wall

®Sea-side impermeable wal

Progress status of dismantling of flange tanks

 To facilitate replacement of flanged tanks, dismantling of flanged tanks started in H1 east/H2 areas in May 2015. Dismantling of all flanged tanks was completed in H1 east area (12 tanks) in October 2015, in H2 area (28 tanks) in March 2016, in H4 area (56 tanks) in May 2017, in H3 B area (31 tanks) in September 2017, in H5 and H5 north areas (31 tanks) in June 2018, in G6 area (38 tanks) in July 2018, H6 and H6 north areas (24 tanks) in September 2018 and G4 south area (17 tanks) in March 2019.





Start of dismantling in H1 east area

After dismantling in H1 east area

Completion of purification of contaminated water (RO concentrated salt water)

Contaminated water (RO concentrated salt water) is being treated using seven types of equipment including the multi-nuclide removal equipment (ALPS). Treatment of the RO concentrated salt water was completed on May 27, 2015, with the exception of the remaining water at the tank bottom. The remaining water will be treated sequentially toward dismantling the tanks.

The strontium-treated water from other facilities than the multi-nuclide removal equipment will be re-purified in the multi-nuclide removal equipment to further reduce risks.

Preventing groundwater from flowing into the Reactor Buildings

Drainage of groundwater by operating the sub-drain pump Pumping well Unit 1

·Length: approx. 1.500m

water flow

(Mountain side→sea

Freezing plant

I and-side

impermeable walls

Reducing groundwater inflow by pumping sub-drain water
To reduce groundwater flowing into the buildings, pumping-up of groundwater from wells
(subdrains) around the buildings started on September 3, 2015. Pumped-up groundwater was
purified at dedicated facilities and released after TEPCO and a third-party organization confirmed
that its quality met operational targets.

Via a groundwater bypass, reduce the groundwater level around the Building and groundwater inflow into the Building

Measures to pump up groundwater flowing from the mountain side upstream of the Building to reduce the groundwater inflow (groundwater bypass) have been implemented.

The pumped up groundwater is temporarily stored in tanks and released after TEPCO and a thirdparty organization have confirmed that its quality meets operational targets.

Through periodical monitoring, pumping of wells and tanks is operated appropriately.

At the observation holes installed at a height equivalent to the buildings, the trend showing a decline in groundwater levels is checked.

The analytical results on groundwater inflow into the buildings based on existing data showed a declining trend.

Installing land-side impermeable walls with frozen soil around Units 1-4 to prevent the inflow of groundwater into the building

To prevent the inflow of groundwater into the buildings, installation of impermeable walls on the land side is planned. Freezing started on the sea side and at a part of the mountain side from March 2016 and at 95% of the mountain side from June 2016. Freezing of the remaining unfrozen sections advanced with a phased approach and freezing of all sections started in August 2017.

In March 2018, construction of the land-side impermeable walls was completed, except for a portion of the depth, based on a monitoring result showing that the underground temperature had declined below 0°C in almost all areas, while on the mountain side, the difference between the inside and outside increased to approx. 4-5 m. The 21st Committee on Countermeasures for Contaminated Water Treatment, held on March 7, 2018, evaluated that together with the function of sub-drains, etc., a water-level management system to stably control groundwater and isolate the buildings from it had been established and had allowed a significant reduction in the amount of contaminated water generated.

For the unfrozen depth, a supplementary method was implemented and it was confirmed that temperature of the part declined below 0°C by September 2018. From February 2019, maintenance operation started at all sections.

Immediate targets

- Reduce the effect of additional release from the entire power station and radiation from radioactive waste (secondary water treatment waste, rubble, etc.) generated after the accident, to limit the effective radiation dose to below 1mSv/year at the site boundaries.
- Prevent contamination expansion in sea, decontamination within the site

Optimization of radioactive protective equipment

Based on the progress of measures to reduce environmental dosage on site, the site is categorized into two zones: highly contaminated area around Unit 1-4 buildings, etc. and other areas to optimize protective equipment according to each category aiming at improving safety and productivity by reducing load during work.

From March 2016, limited operation started. From March and September 2017, the G Zone was expanded.



R zone	Y zone	G zone	
(Anorak area)	(Coverall area)	(General wear)	
Full-face mask	Full-face or half-face masks *1 *2	Disposable disposable mask	
Anorak on coverall		General*3 Dedicated on-site wear	
Or double coveralls	Coverall		

- *1 For works in buildings including water-treatment facilities [multi-nuclide removal equipment, etc.] (excluding site visits), wear a full-face mask.
- "2 For works in tank areas containing concentrated salt water or Sr-treated water (excluding works not handling concentrated salt water, etc., patrol, on-site investigation for work planning,
- and site visits) and works related to tank transfer lines, wear a full-face mask. 3 Specified light works (patrol, monitoring, delivery of goods brought from outside, etc.



Installation of dose-rate monitors

To help workers in the Fukushima Daiichi Nuclear Power Station precisely understand the conditions of their workplaces, a total of 86 dose-rate monitors were installed by January 4, 2016.

These monitors allow workers to confirm real time on-site dose rates at their workplaces.

Workers are also able to check concentrated data through large-scale displays installed in the Main Anti-Earthquake Building and the access control facility.



Installation of Dose-rate monitor

Installation of sea-side impermeable walls

To prevent the outflow of contaminated water into the sea, sea-side impermeable walls have been installed.

Following the completed installation of steel pipe sheet piles on September 22, 2015, connection of these piles was conducted and connection of sea-side impermeable walls was completed on October 26, 2015. Through these works, closure of sea-side impermeable walls was finished and the contaminated water countermeasures have been greatly advanced.



Installation of steel pipe sheet piles for sea-side impermeable wall

Status of the large rest house

A large rest house for workers was established and its operation commenced on May 31, 2015.

Spaces in the large rest house are also installed for office work and collective worker safety checks as well as taking rest.

On March 1, 2016 a convenience store opened in the large rest house. On April 11, operation of the shower room started. Efforts will continue to improve convenience of workers.

